

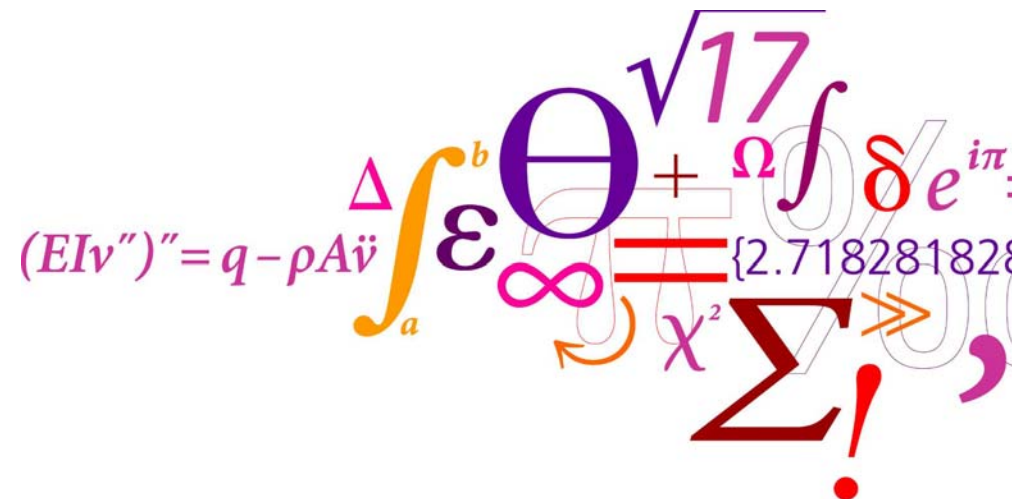
Model for Environmental Assessment of Container Ship Transport

By

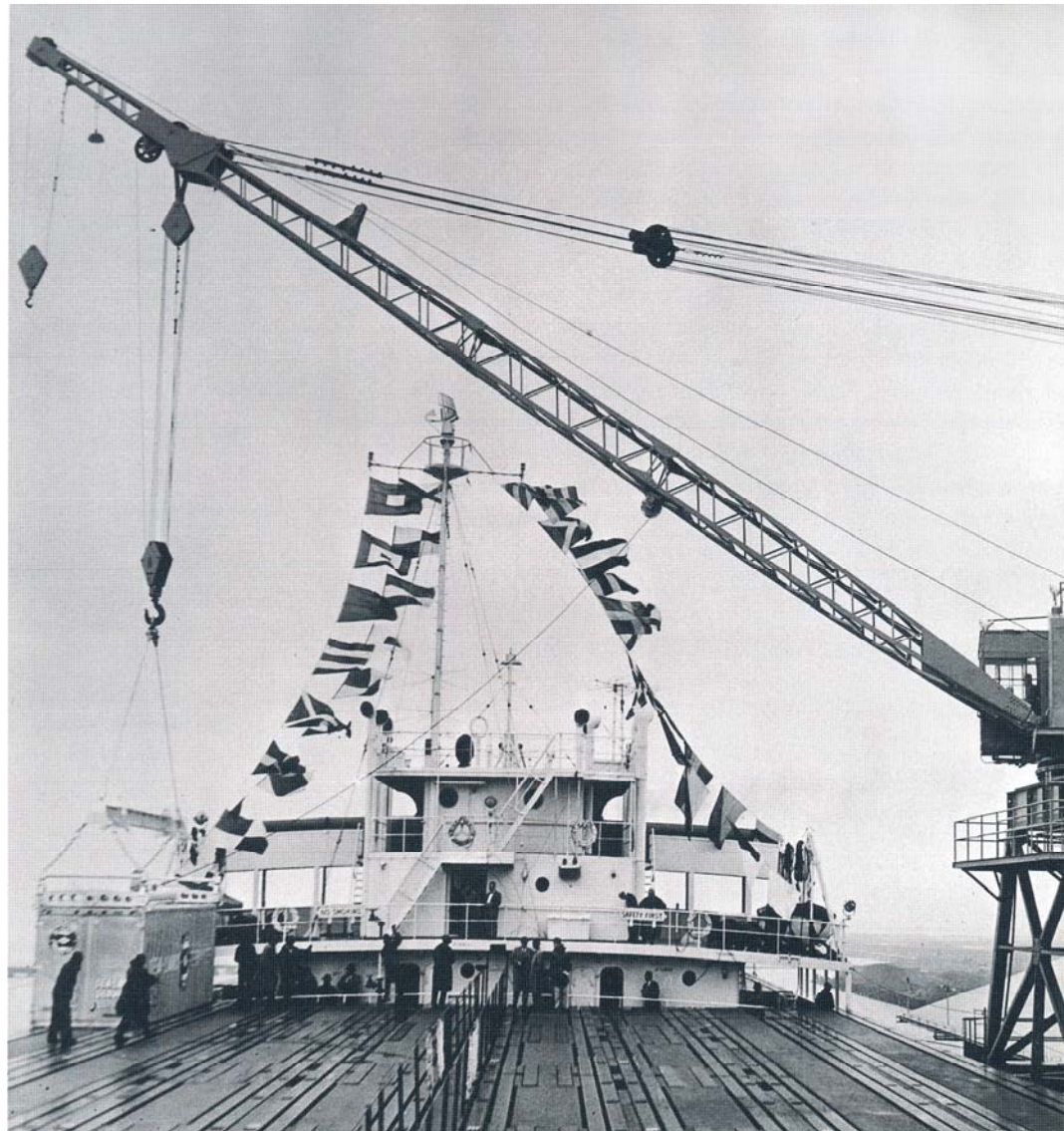
Hans Otto Holmegaard Kristensen

Senior researcher

Technical University of Denmark



1956 – Ideal X (Malcom McLean)



2006 – EMMA MAERSK (14770 TEU)



Overview of presentation



1. Basic principles of model
2. Identification of critical parameters which influence EEDI
3. Basic principles of calculation model
4. The most important parameter: **SPEED OF THE SHIP**
5. Result of parameter analysis
6. Possible EEDI improvements
7. Summary/conclusion

EEDI definition

The Energy Efficiency Design Index (EEDI) is a measure of the CO₂ efficiency of a ship. It is calculated according to the following formula in its most simple formulation:

$$\text{EEDI} = \frac{P_{ME} \times \text{SFC}_{ME} \times C_{FME} + P_{AE} \times \text{SFC}_{AE} \times C_{FAE}}{\text{Deadweight} \times \text{Speed}}$$

P_{ME} and P_{AE} is main engine and auxiliary engine power

The basic principle of EEDI is that it expresses the CO₂ emissions per unit of the transport work of the ship.

SFC is the certified specific fuel consumption [g/kW/hour] of the engines.

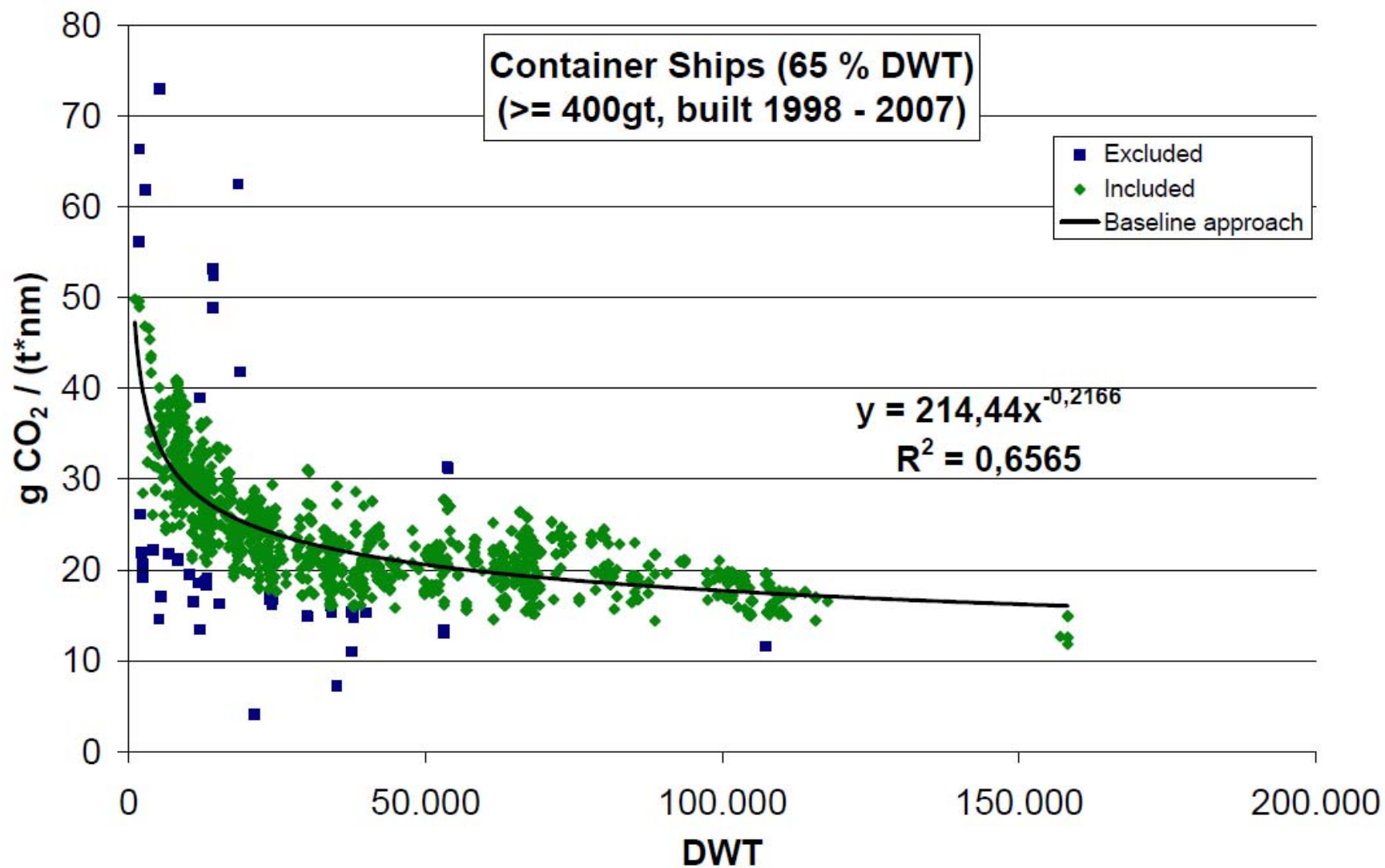
C_F is a non-dimensional conversion factor between fuel consumption and CO₂ emission

Main objective: Minimise EEDI

$$\text{EEDI} = \frac{P_{ME} \times \text{SFC}_{ME} \times \text{CF}_{ME} + P_{AE} \times \text{SFC}_{AE} \times \text{CF}_{AE}}{\text{Capacity} \times \text{Speed}}$$

$$\text{EEDI} = \frac{\text{Constant} \times P_{ME}}{\text{Capacity} \times \text{Speed}}$$

EEDI base line (MEPC 60/4/14)



Specific oil consumption and emissions

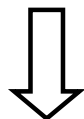
$$\frac{\text{Oil consumption}}{\text{Transport unit}} = \frac{\text{Engine power} \times \text{specific oil cons.}}{\text{Transport capacity} \times \text{speed}}$$

Calculation methods:

1. 'Bottom up' (pure statistical method)
2. 'Top down method' (model calculation – naval architectural method)

First calculate ship length, L, as function of cargo capacity, C

$$L = f_0(C)$$



On basis of statistical data calculate the ship's dimensions as functions of ship length, L

$$\text{Beam} = B = f_1(L)$$

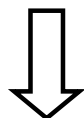
$$\text{Draft} = T = f_2(L)$$

$$\text{Depth} = D = f_3(L)$$

$$\text{Light ship weight} = M = f_4(L)$$

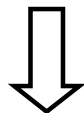
$$\text{Service speed} = V = f_5(L)$$

$$\text{Auxiliary machinery power} = P_a = f_6(L)$$



Propulsion power, P_f , is calculated on the basis of main dimensions, cargo capacity, C, and utilization fraction, U (actual cargo/maximum cargo capacity)

$$P_f = f_7(L, B, T, D, M, V, C, U)$$



Energy consumption and emissions are calculated on the basis of the propulsion and auxiliary power P_f and P_a

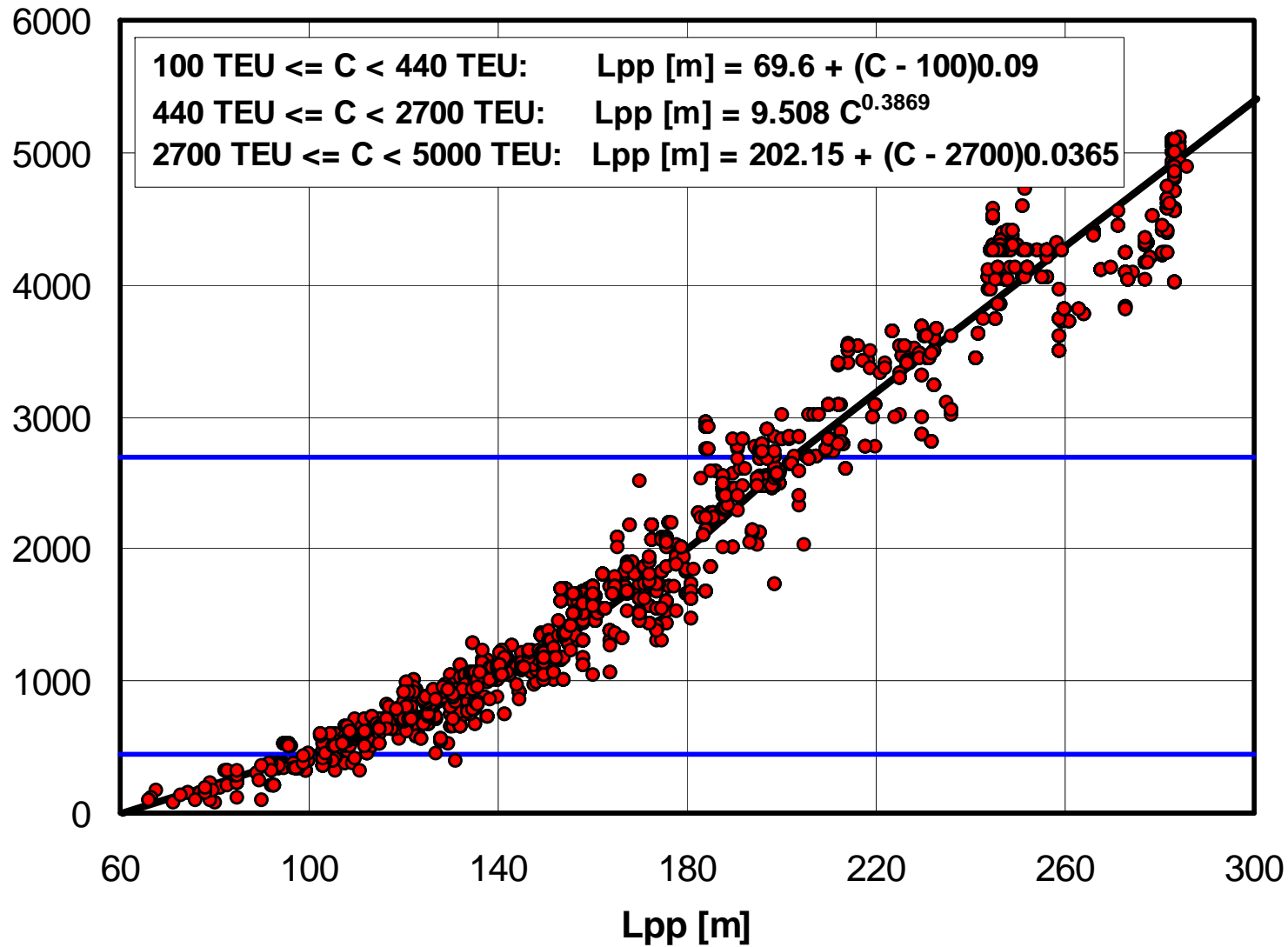
Finally, main dimensions can be modified and their influence on propulsion power and energy consumption can be determined

**Principles
of
calculation
model**

Panamax ships – Lpp versus TEU capacity



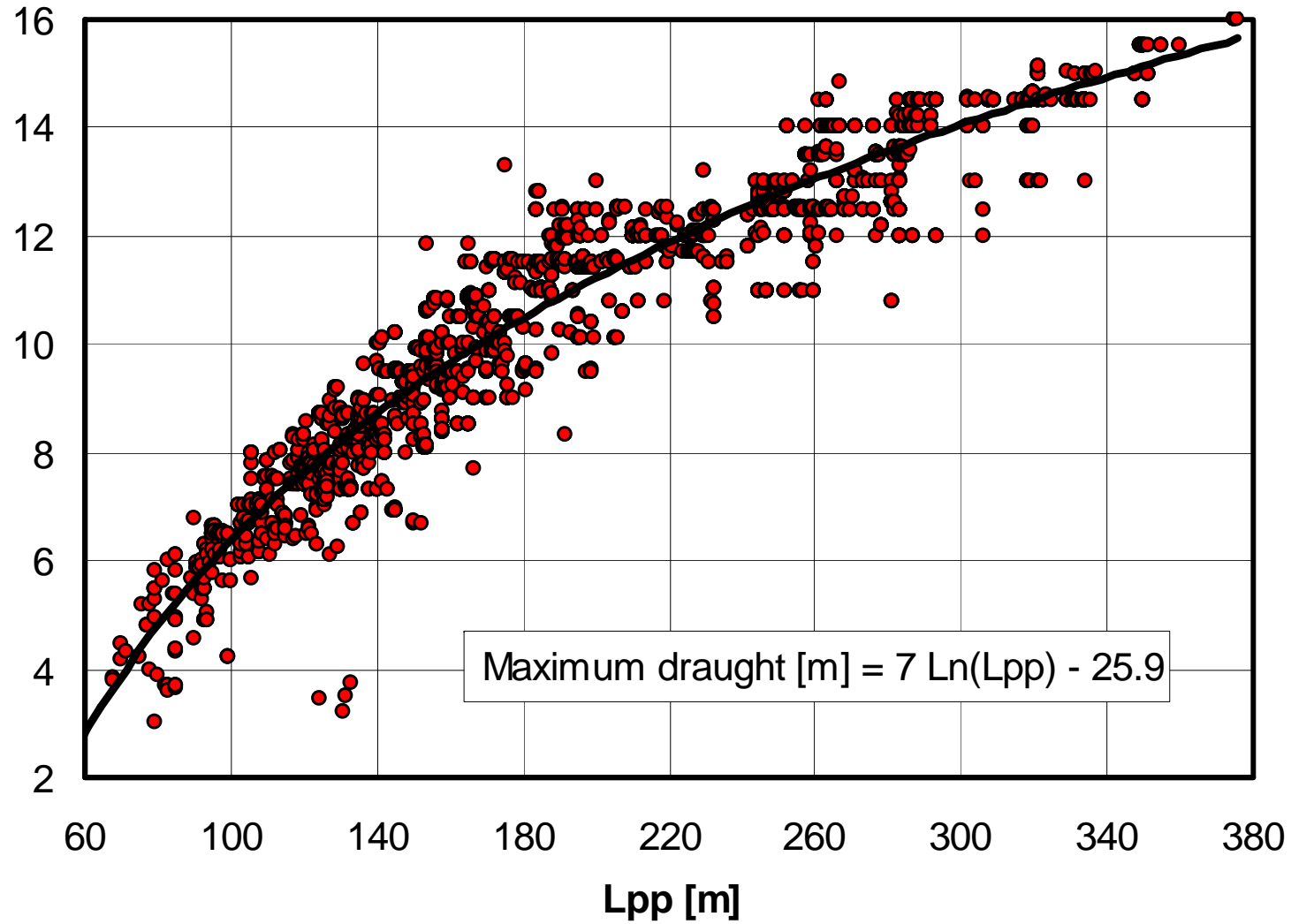
Capacity [TEU]



Maximum draught versus Lpp



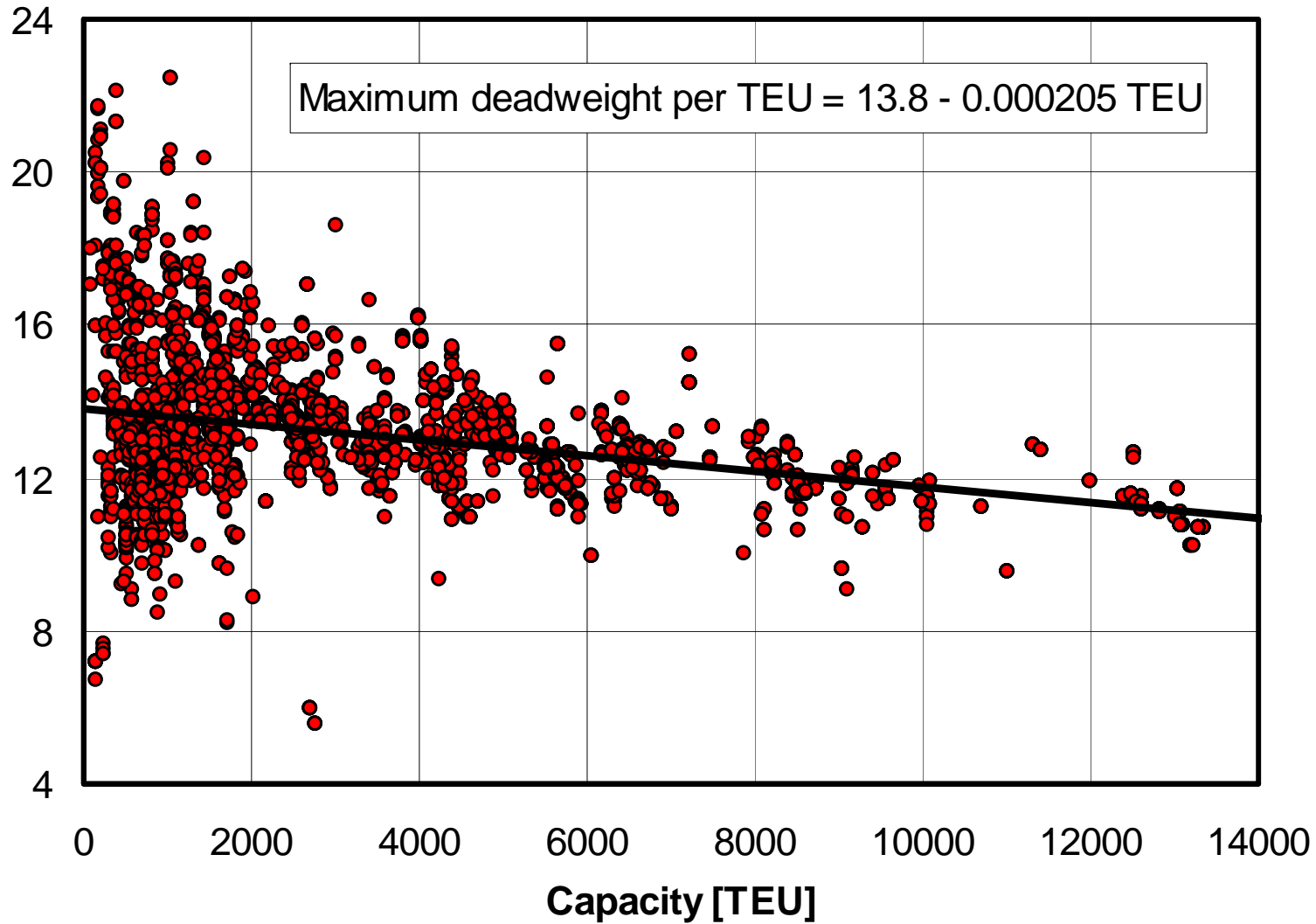
Draught [m]



Maximum DWT/TEU versus Lpp



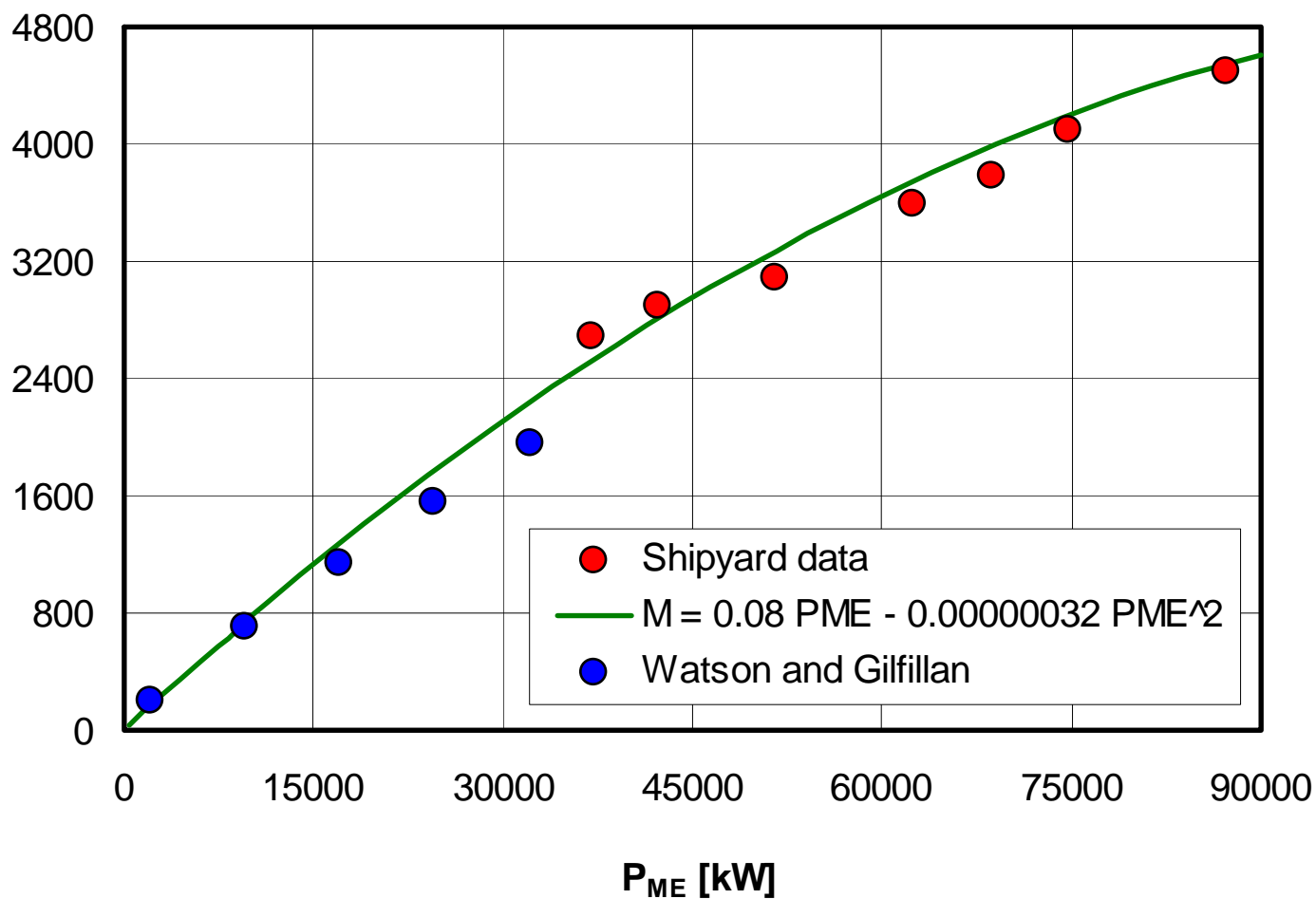
Dwt per TEU



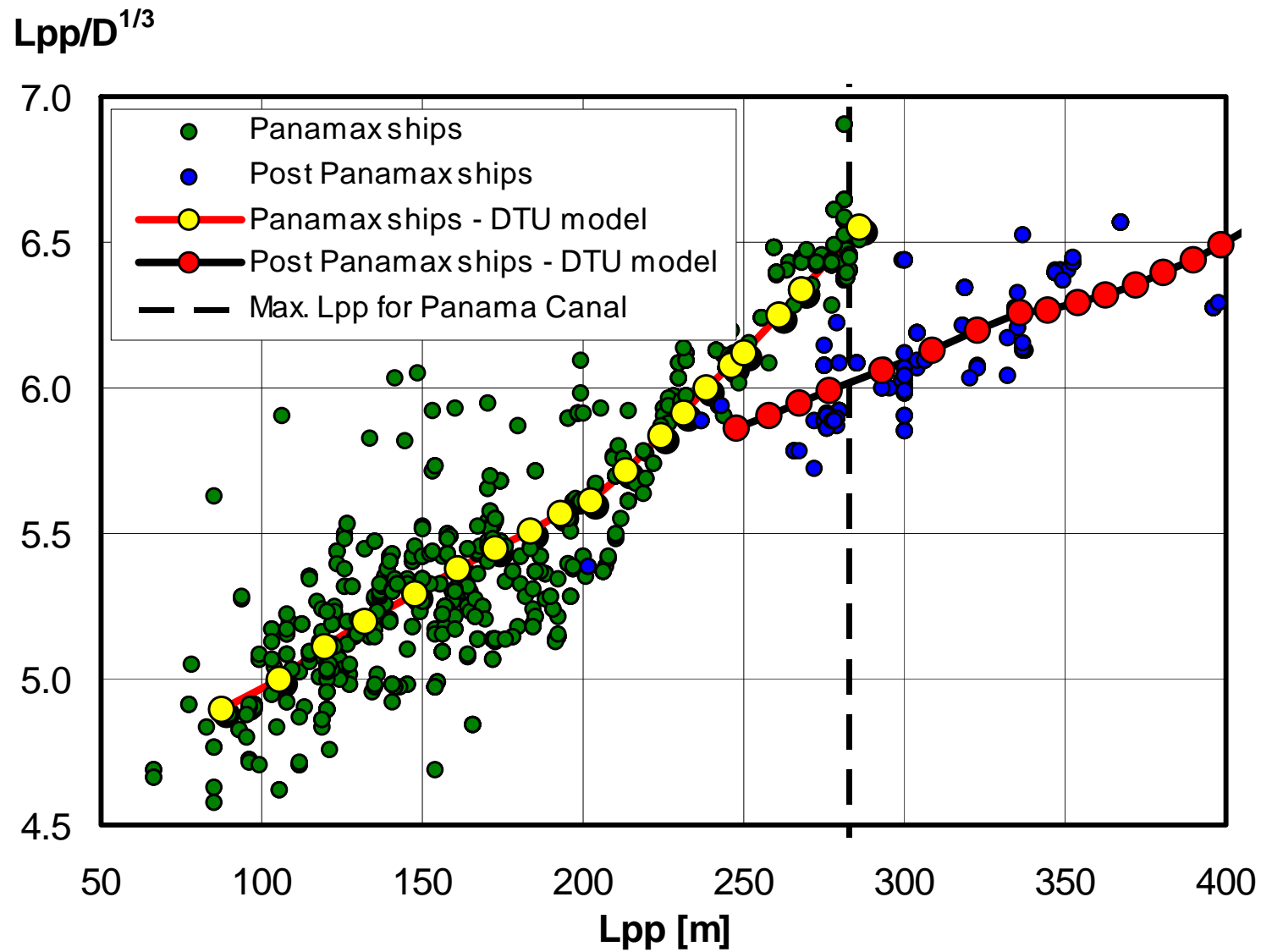
Machinery weight for container ships

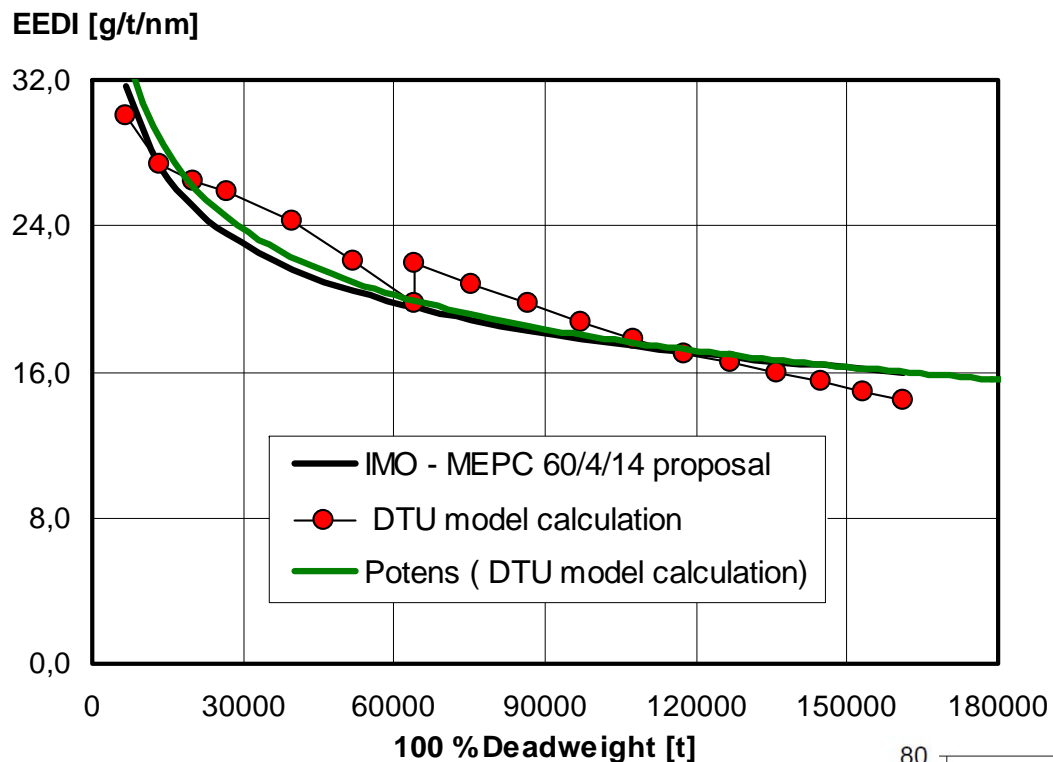
Machinery weight [t]

$$\text{Machinery weight [t]} = 0.08 P_{ME} - 0.00000032 P_{ME}^2$$

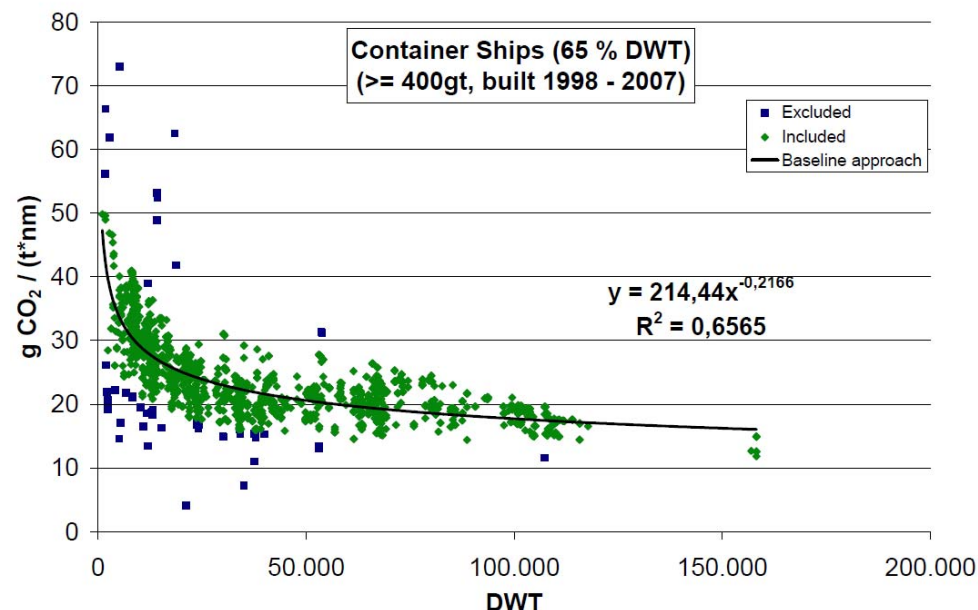


Slenderness ratio – $L_{pp}/Displ.volumue^{1/3}$

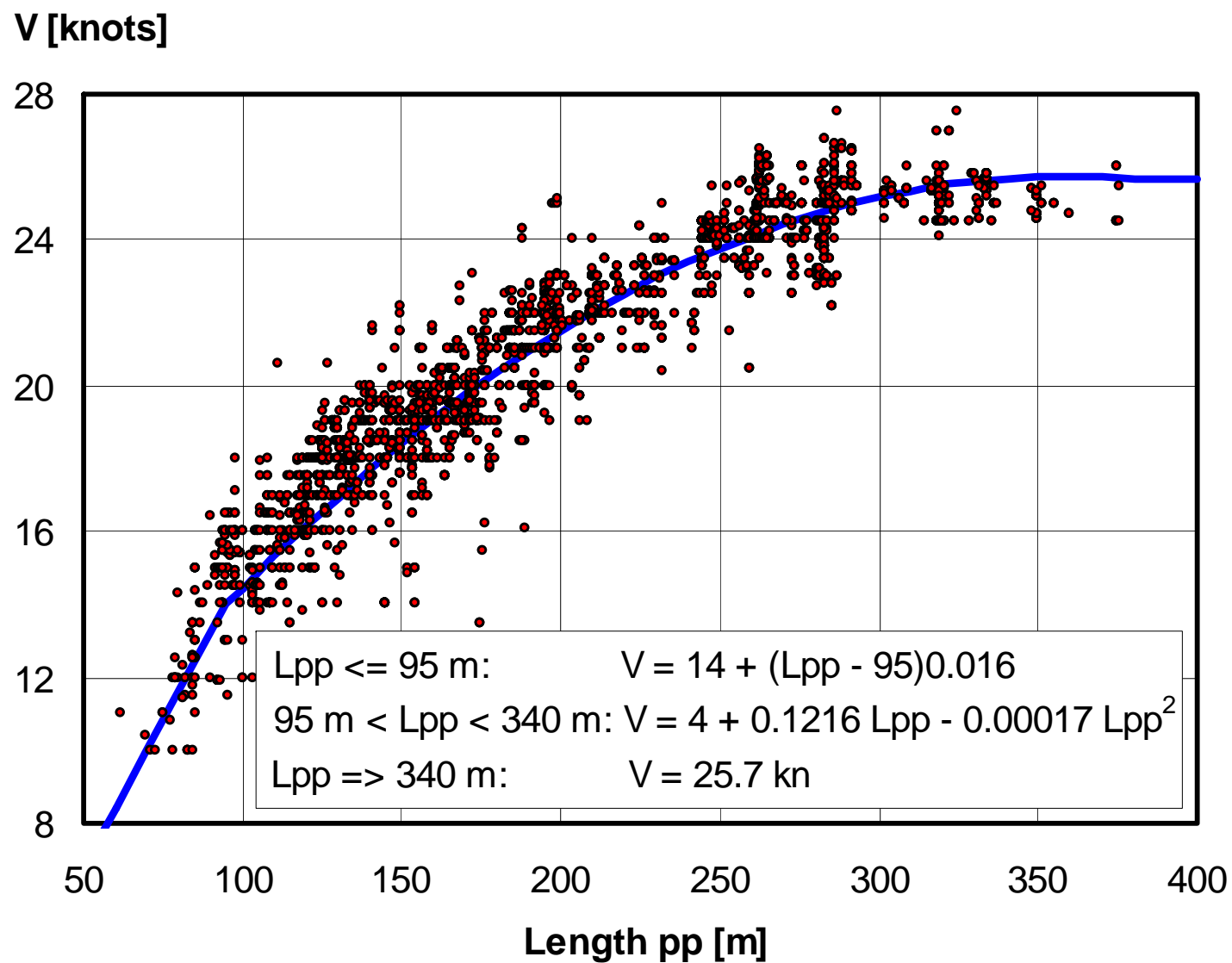




**EEDI
model data
versus
IMO baseline**



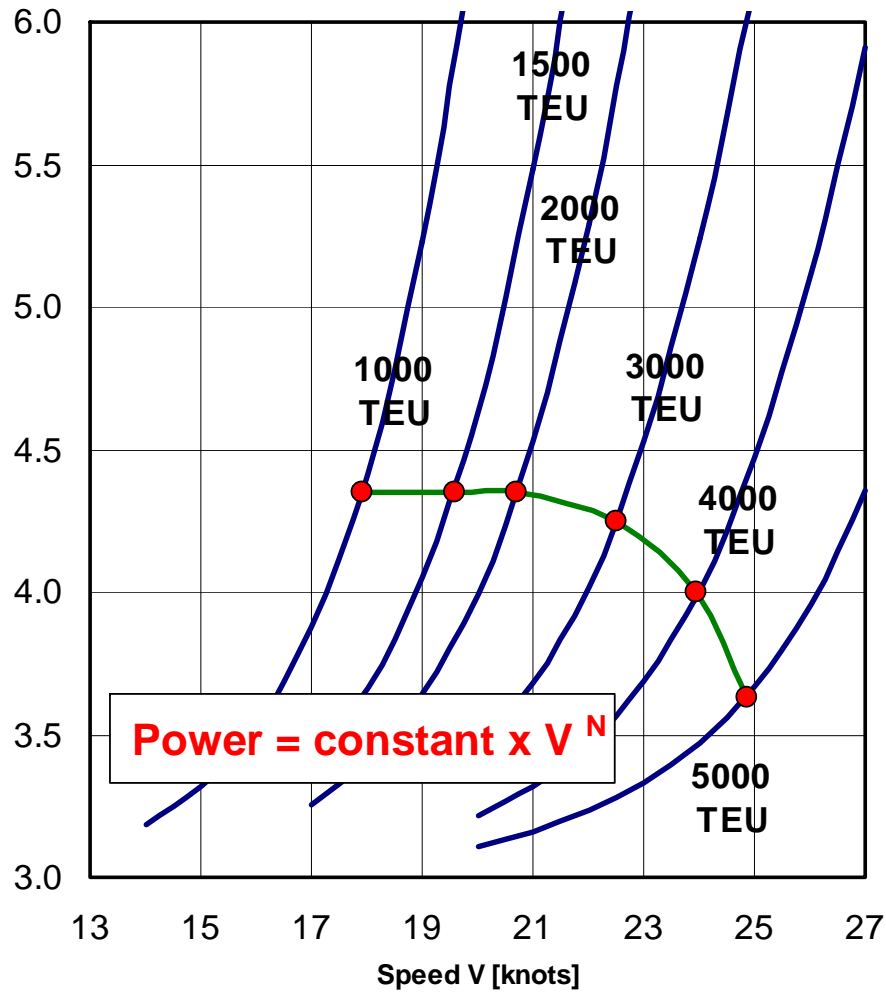
Speed



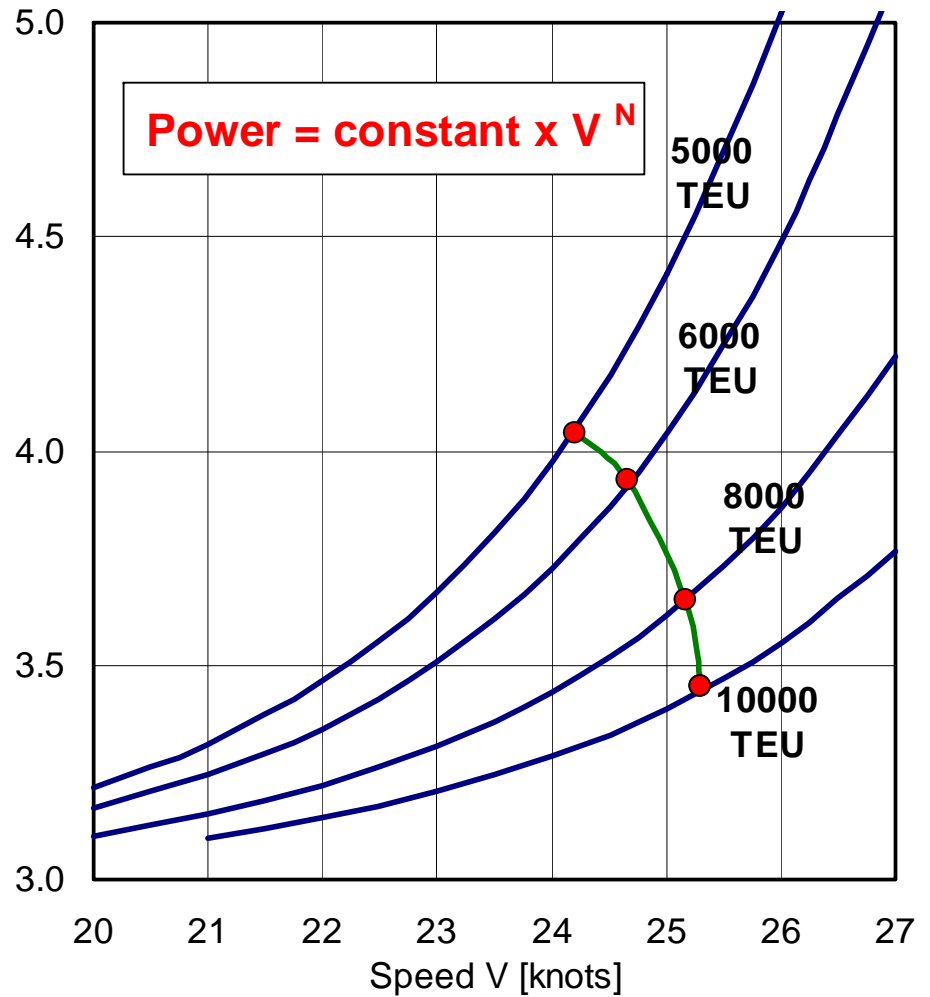
Speed exponent N



Speed exponent N



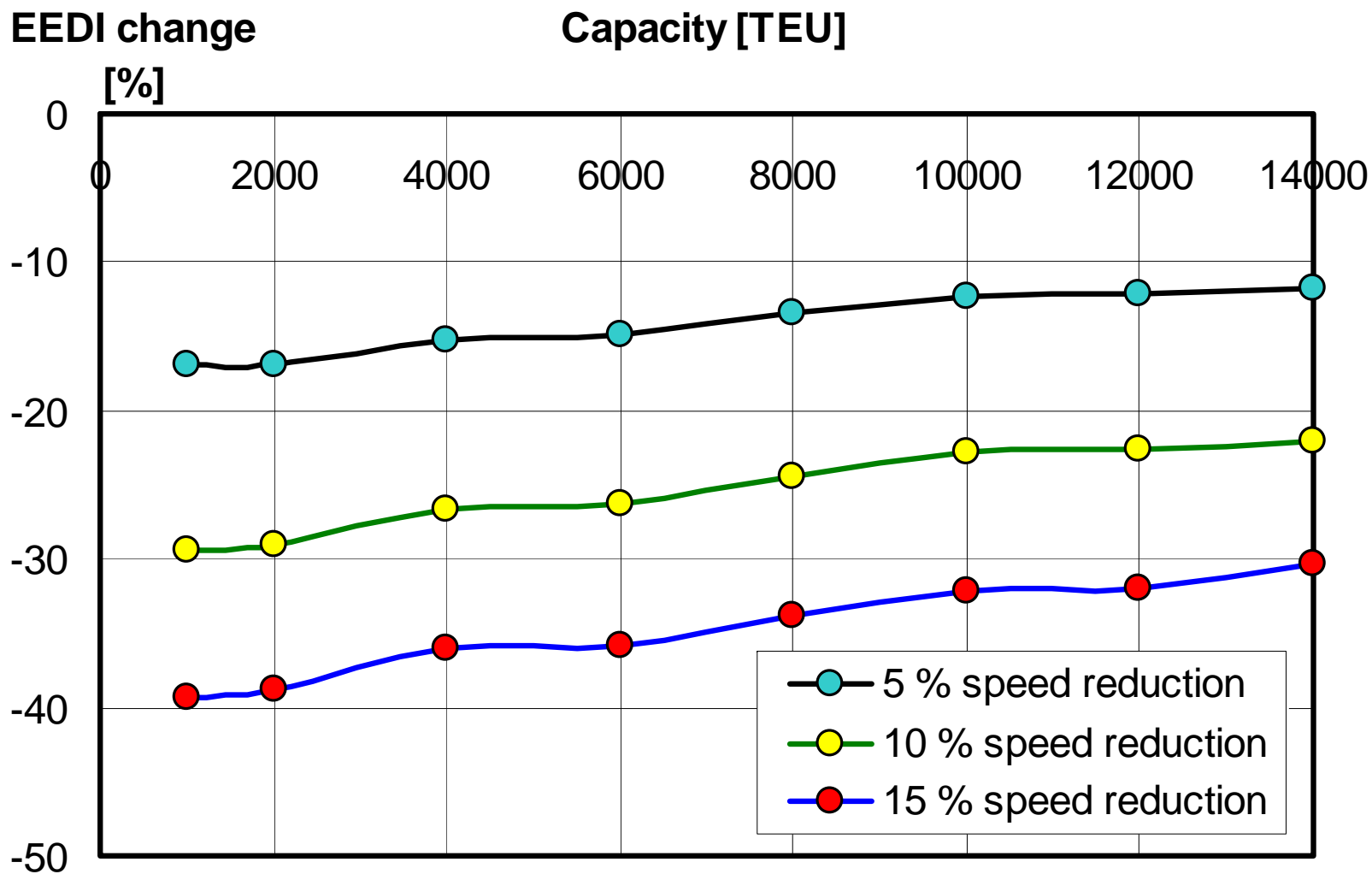
Speed exponent N



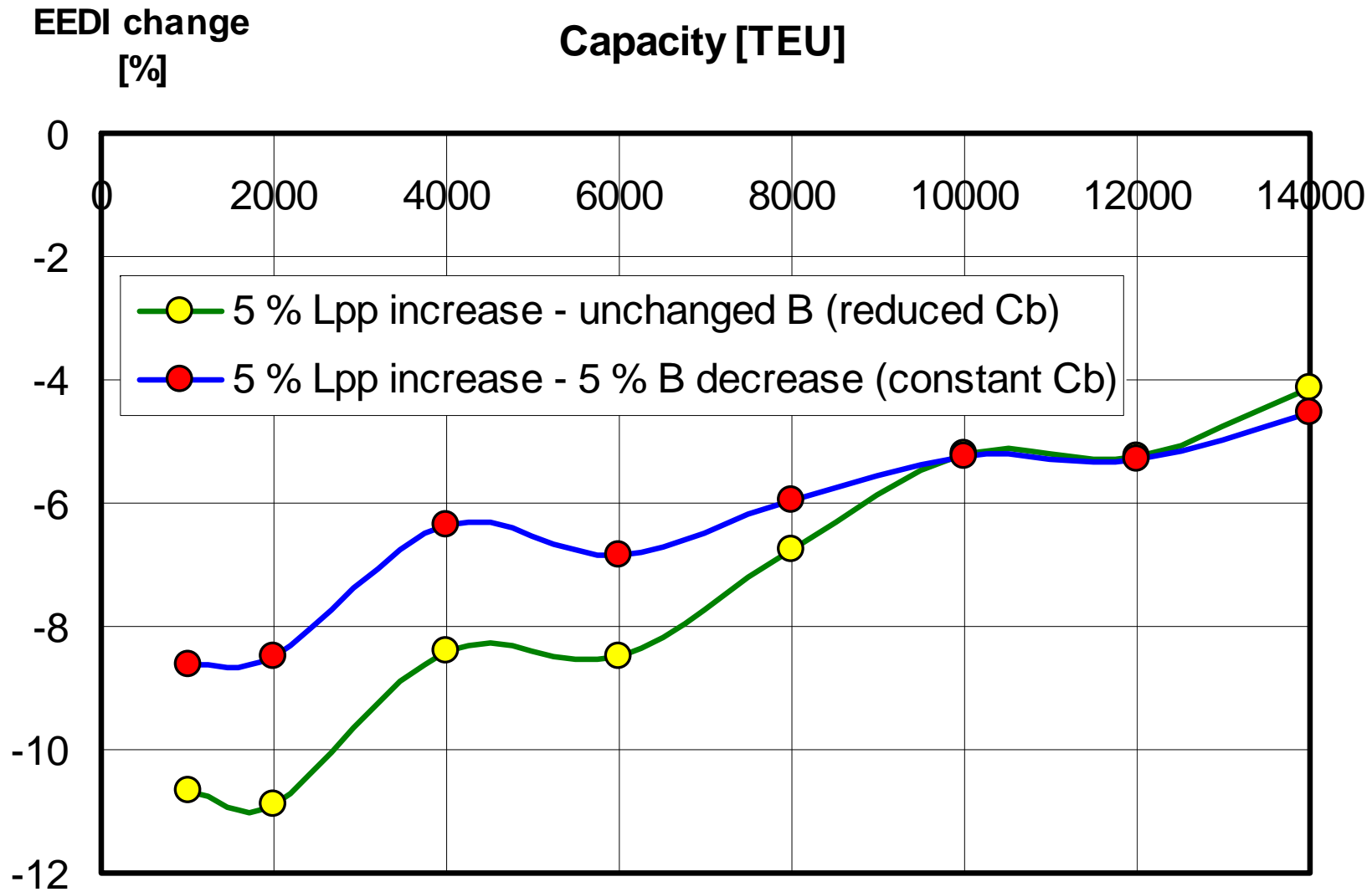
EEDI and speed

$$\text{EEDI} = \frac{\text{Constant} \times \text{Power}}{\text{Transport capacity} \times \text{speed}} = \frac{\text{Constant} \times \text{speed}^N}{\text{Transport capacity} \times \text{speed}} = \frac{\text{Constant} \times \text{speed}^{(N-1)}}{\text{Transport capacity}}$$

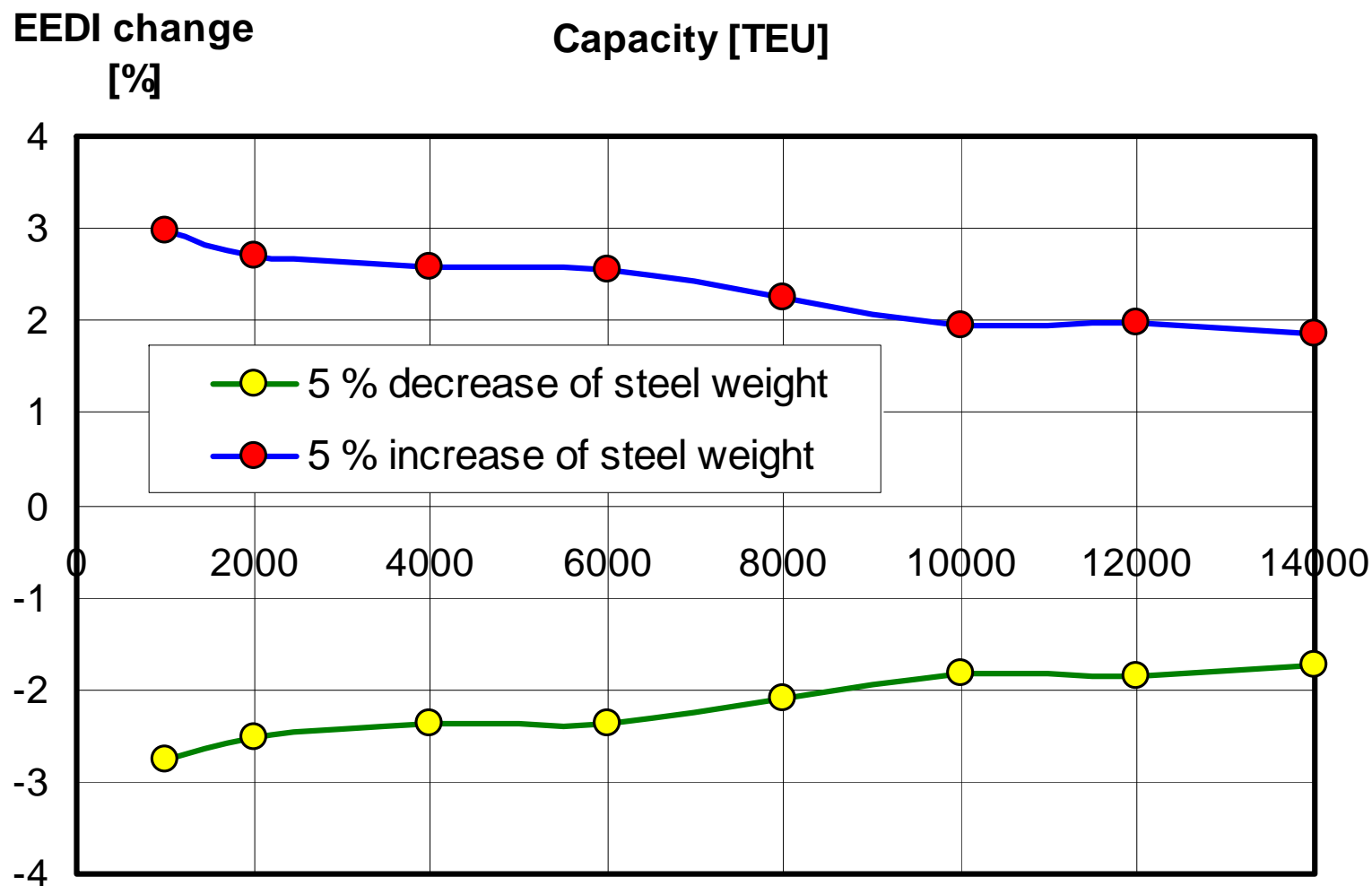
Influence of speed on EEDI



EEDI reduction by increased ship length



EEDI reduction by changed steel weight



Obtainable EEDI reductions



Design option for improvement of EEDI	4000 TEU	8000 TEU	12000 TEU
Ship designed for normal service speed with 10 % sea margin on resistance and ME engine running 90 % MCR in service condition	0	0	0
Ship designed for normal service speed with NO sea margin on resistance and ME engine running 90 % MCR in service condition	8	8	8
Ship designed for normal service speed with NO sea margin on resistance and derated ME engine running 100 % in service condition	17	17	16
5 % lengthened ship designed for normal service speed with NO sea margin on resistance and derated ME engine running 100 % MCR in service condition	24	22	21
5 % lengthened ship designed for 10 % speed reduction with NO sea margin on resistance and derated ME engine running 100 % MCR in service condition	41	39	37
5 % lengthened ship designed for 10 % speed reduction with NO sea margin on resistance and derated ME engine running 100 % MCR in service condition. 3 % steel weight reduction	41	40	38
5 % lengthened ship designed for 10 % speed reduction with NO sea margin on resistance and derated ME engine running 100 % MCR in service condition. 3 % steel weight reduction and 5 % improved propeller efficiency	44	42	41

Summary of EEDI reductions (No change of sea margin)



Option 1:

Use of derated engine

3 % steel weight optimization

5 % propulsion improvement

20 – 23 % EEDI reduction

Option 2:

Use of derated engine

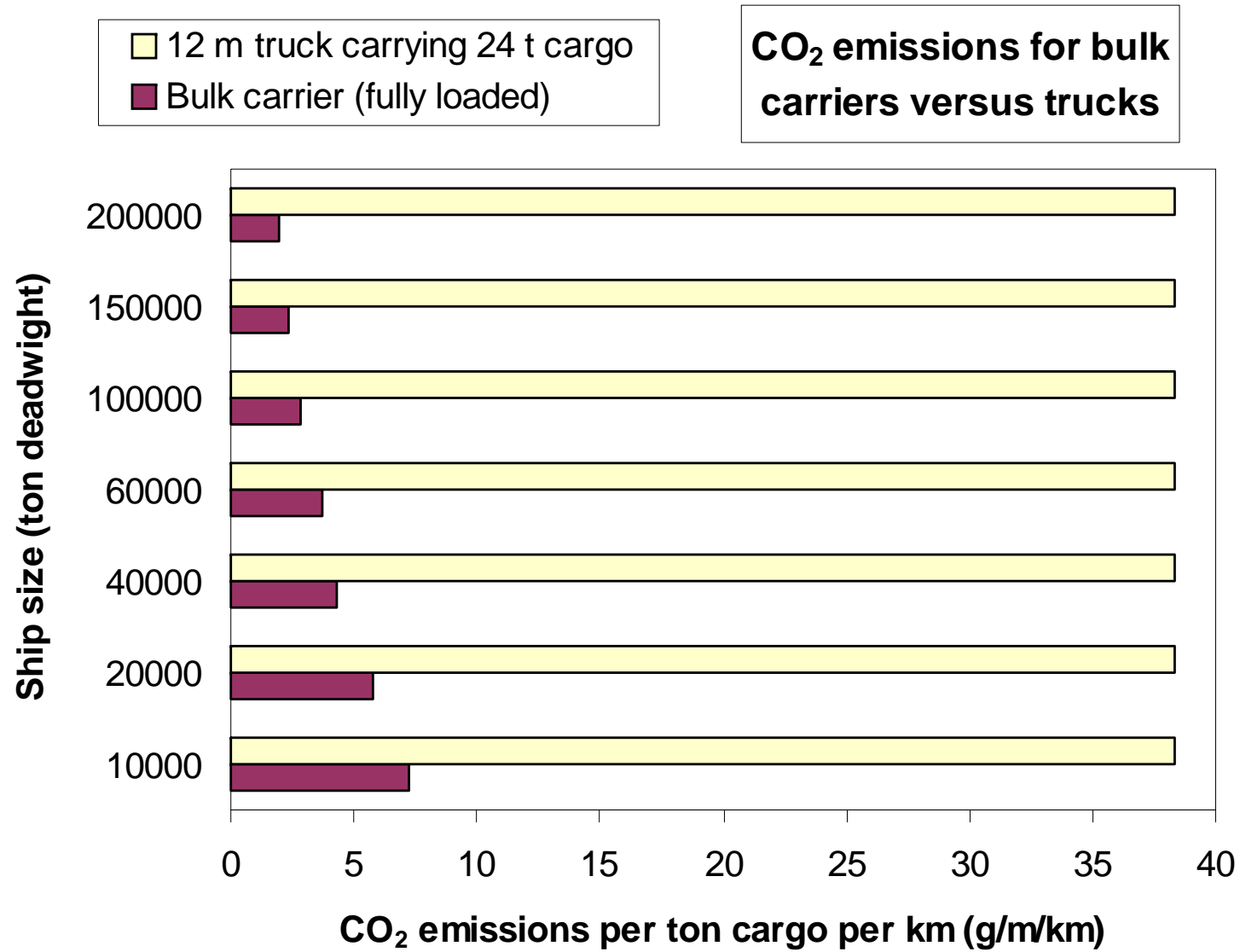
3 % steel weight optimization

5 % propulsion improvement

10 % speed reduction

37 – 42 % EEDI reduction

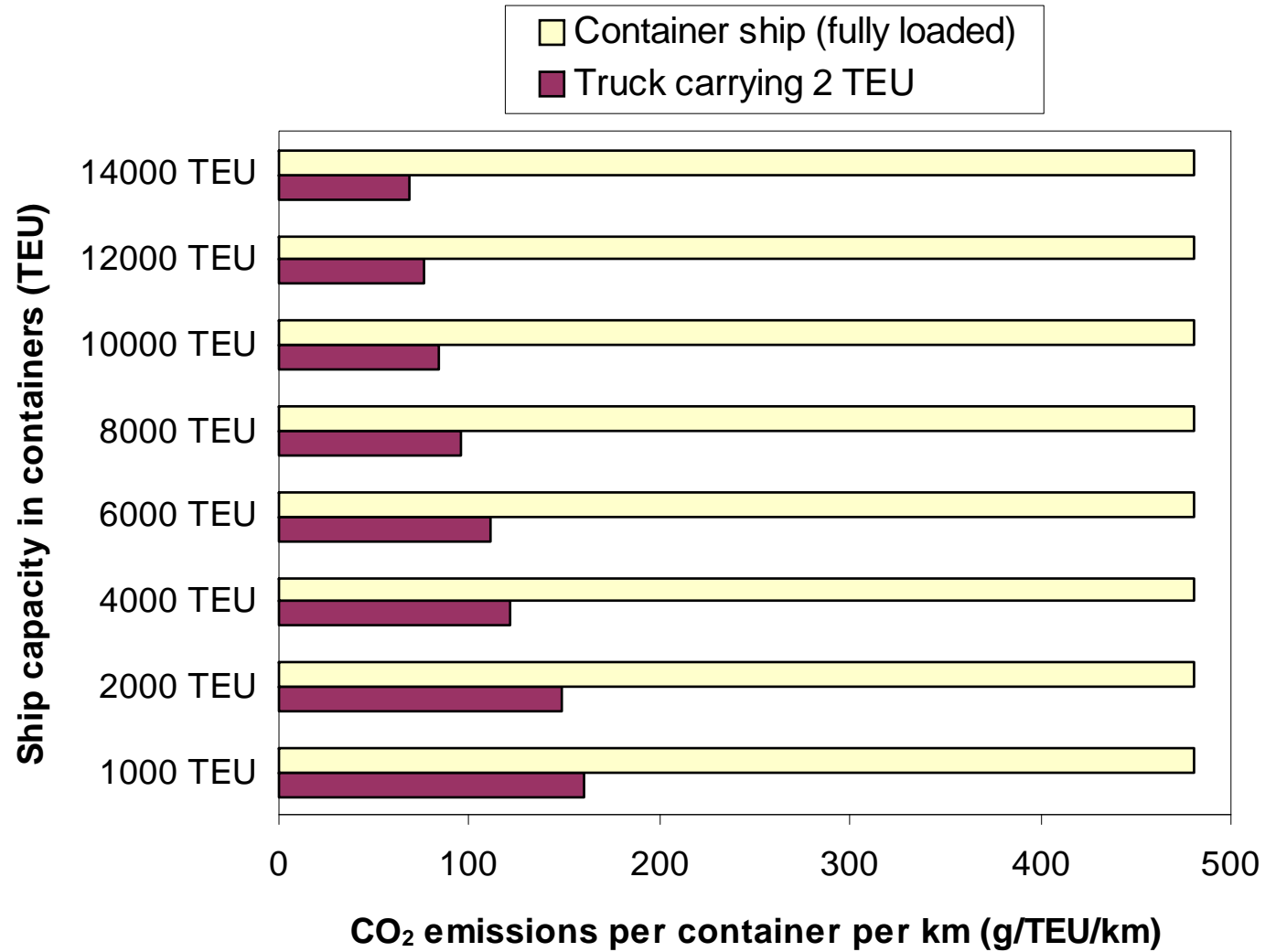
CO₂ emissions for ships versus trucks



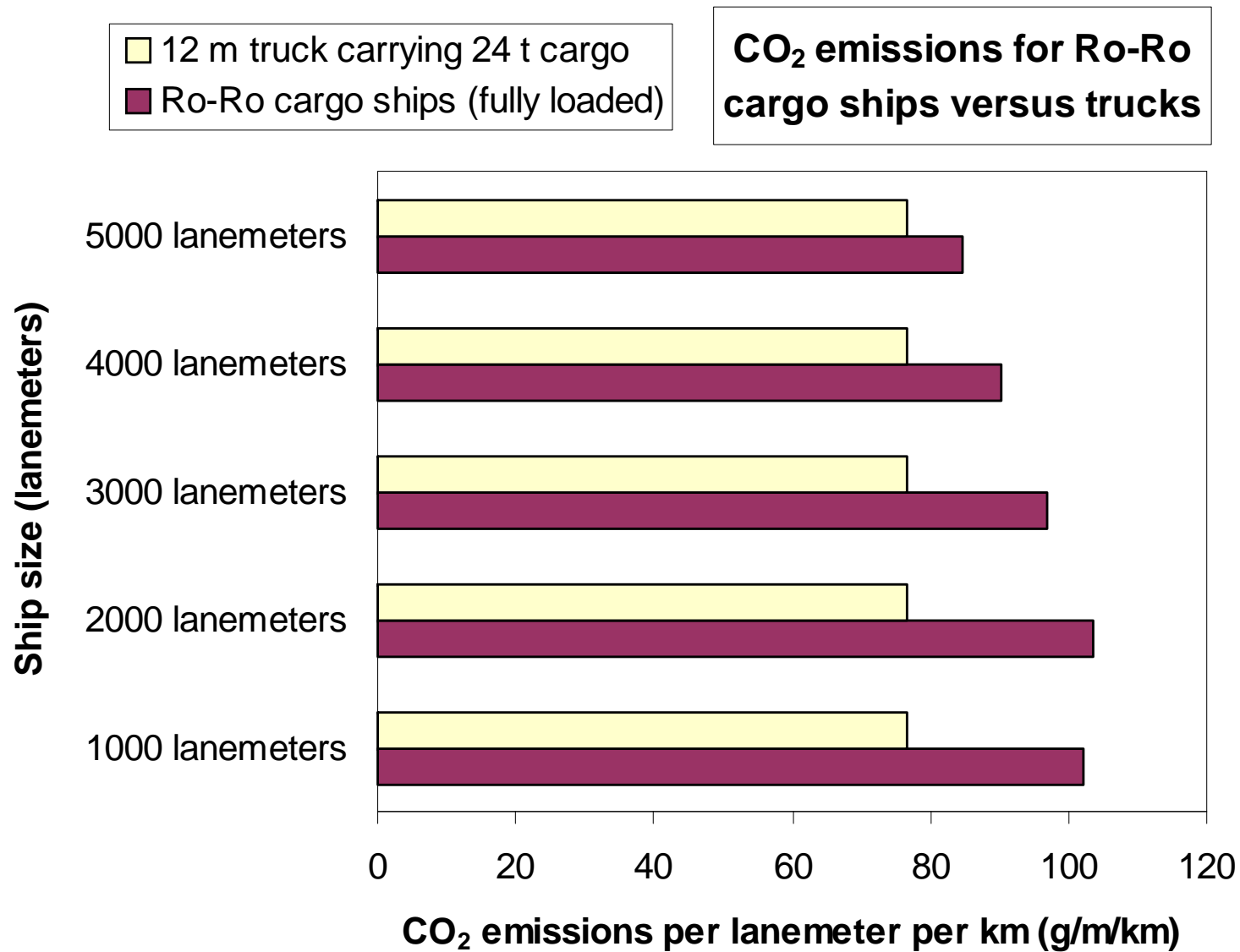
CO₂ emissions for ships versus trucks



CO₂ emissions for container ships versus trucks



CO₂ emissions for ships versus trucks



Thank you !